

1 **USING THE NAVIER-CAUCHY EQUATION FOR MOTION**
2 **ESTIMATION IN DYNAMIC IMAGING**

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ABSTRACT. Tomographic image reconstruction is well understood if the specimen being studied is stationary during data acquisition. However, if this specimen changes its position during the measuring process, standard reconstruction techniques can lead to severe motion artefacts in the computed images. Solving a dynamic reconstruction problem therefore requires to model and incorporate suitable information on the dynamics in the reconstruction step to compensate for the motion.

Many dynamic processes can be described by partial differential equations which thus could serve as additional information for the purpose of motion compensation. In this article, we consider the Navier-Cauchy equation which characterizes small elastic deformations and serves, for instance, as a simplified model for respiratory motion. Our goal is to provide a proof-of-concept that by incorporating the deformation fields provided by this PDE, one can reduce the respective motion artefacts in the reconstructed image. To this end, we solve the Navier-Cauchy equation prior to the image reconstruction step using suitable initial and boundary data. Then, the thus computed deformation fields are incorporated into an analytic dynamic reconstruction method to compute an image of the unknown interior structure. The feasibility is illustrated with numerical examples from computerized tomography.

3 **1. Introduction.** Imaging modalities represent a well-known application of the
4 theory of inverse problems. If the specimen is stationary during the data collec-
5 tion, the reconstruction process is well understood for most imaging systems [36].
6 A dynamic behaviour of the object during measurement, however, results in incon-
7 sistent data, and standard reconstruction techniques derived under the stationary
8 assumption lead to severe motion artefacts in the computed images [13, 31, 42].
1 This affects medical applications, for instance due to respiratory motion, as well as

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2 non-destructive testing while imaging driven liquid fronts for oil recovery studies [3]
3 or while performing elasticity experiments during the scan to determine material
4 parameters [25].

5 An intuitive approach for the case of few but consistent data would be to consider
6 a quasi-static framework. However, this is only applicable if the object motion is
7 sufficiently slow compared to the overall data acquisition time or if the motion is
8 periodic. Solving the dynamic reconstruction problem in general requires to model
9 and incorporate dynamical prior information within the reconstruction step. For
10 individual imaging modalities like computerized tomography, magnetic resonance
11 imaging or positron emission tomography, several methods of this type have been
12 proposed in the literature, based on rebinning or gating the data [46, 33, 15], a
13 variational formulation [14, 37, 32, 6], exact analytic methods [11, 12, 20], iterative
14 procedures [2, 24] or approximate inversion formulas [26, 27, 17]. Further, reg-
15 ularization techniques developed in the general context of dynamic linear inverse
16 problems [29, 16, 40, 41, 8] have been successfully applied to imaging problems.

17 The most efficient way to compensate for the dynamics is to model and incorpo-
18 rate the motion prior in form of a deformation map Φ which describes the trajectory
19 of the particles in the interior of the object over time. In general, such deforma-
20 tion fields are a priori unknown and have to be extracted from the measured data.
21 Typically, parametrized motion models are employed, i.e. only a few unknown pa-
22 rameters need to be estimated, either via additional measurements [11, 2, 34, 39]
23 or directly from the recorded tomographic data. In computerized tomography, for
24 instance, they can be determined by detecting traces of nodal points in the sino-
25 gram [33, 17]. For global rotations and translations, an estimation procedure using
26 data consistency conditions is proposed in [48]. Iterative procedures are, for ex-
27 ample, based on edge entropy [28], or perform estimation and reconstruction step
28 simultaneously [45].

29 Alternatively, the dynamics can be characterized in terms of velocity fields be-
30 tween consecutive image frames. The intensity variations in the image sequence
31 are then linked to the underlying velocity field by the optical flow constraint, based
32 on the brightness constancy assumption. Recovering both velocity fields and image
33 frames from the measured data simultaneously requires solving non-convex opti-
34 mization problems of extremely large size [4, 5].

35 In this article, we pursue another approach. Many dynamic processes can be de-
36 scribed by partial differential equations, and thus, their (numerical) solution could
37 provide the required deformation fields. More precisely, we consider in the follow-
38 ing the Navier-Cauchy equation, representing linear elasticity. In applications in
39 radiotherapy treatment planning, the respective conservation laws are employed to
40 model respiratory motion [47].

41 To reduce the overall complexity and to provide a proof-of-concept that such
42 motion priors can compensate for the dynamics, we suggest to decouple both tasks
43 for the study in this article. Based on the provided results, the study of the joint
44 parameter identification problem will then be subject to future work.

45 In Section 2, we recall the mathematical model of dynamic imaging and present
46 the general motion compensation strategy from [18] in the mass preserving case
47 which assumes that the motion is known. We then derive our elastic motion model
48 based on conservation laws in Section 3. The respective model in particular requires
49 prescribed initial and boundary data. Therefore, we discuss suitable choices which

1 are feasible regarding practical applications. The numerical calculation of the de-
 2 formation fields is studied in Section 4. Finally, the potential of the motion model
 3 for the purpose of motion compensation is illustrated in Section 5 at the exam-
 4 ple of computerized tomography, combining the numerically computed deformation
 5 fields with our dynamic reconstruction strategy. We conclude with an outlook to
 6 expand the suggested approach towards determining an unperturbed image and the
 7 deformation fields simultaneously via a joint parameter identification problem.

8 **2. Models and reconstruction strategies in dynamic imaging.** In this sec-
 9 tion, we introduce the mathematical framework to formulate and address the prob-
 10 lem of dynamic image reconstruction. In particular, we will consider the two-
 11 dimensional case throughout the article. Further, since the motion estimation
 12 approach via the Navier-Cauchy equation is not restricted to a particular imag-
 13 ing modality, we want to present the motion compensation strategy in a framework
 14 covering many different modalities. A detailed introduction can be found for in-
 15 stance in [16, 18].

16 We start by deriving the model of the stationary setting. To be more intuitive,
 17 we first consider the example of computerized tomography (CT). In CT, X-ray
 18 beams are transmitted through the specimen of interest to a detector where the
 19 intensity loss of the X-rays is recorded. In particular, the radiation source needs
 20 to rotate around the object to capture information from different angles of view.
 21 Due to this rotation, the data acquisition takes a considerable amount of time. The
 22 mathematical model for this imaging process is given by the Radon transform

$$\mathcal{R}h(t, y) = \int_{\mathbb{R}^2} h(x) \delta(y - x^T \theta(t)) dx, \quad (t, y) \in [0, 2\pi] \times \mathbb{R}, \quad (1)$$

which integrates h along the straight lines $\{x \in \mathbb{R}^2 : x^T \theta(t) = y\}$, i.e. along the
 path of the emitted X-rays. In particular, the unit vector $\theta(t) = (\cos(t), \sin(t))^T$
 characterizes the source position at time instance t , while y denotes the affected
 detector point, and δ stands for the delta distribution. The goal is then to recover
 h , the linear attenuation coefficient of the studied specimen, from measurements
 $g(t, y) = \mathcal{R}h(t, y)$ with $(t, y) \in [0, 2\pi] \times \mathbb{R}$. Using the Fourier transform of δ , we
 further obtain the equivalent representation

$$\mathcal{R}h(t, y) = \int_{\mathbb{R}} \int_{\mathbb{R}^2} (2\pi)^{-1/2} e^{i\sigma(y - x^T \theta(t))} h(x) dx d\sigma.$$

Besides CT, many imaging modalities in the stationary setting can be mod-
 eled mathematically by a linear operator which integrates the searched-for quantity
 along certain manifolds, for instance along circles, respectively spheres, in SONAR
 or photoacoustic tomography. Thus, we consider in the following a more general
 framework, namely model operators of type

$$\mathcal{A}h(t, y) = \int_{\mathbb{R}} \int_{\Omega_x} h(x) a(t, y, x) e^{i\sigma(y - H(t, x))} dx d\sigma, \quad (t, y) \in \mathbb{R}_T \times \Omega_y, \quad (2)$$

23 where Ω_x and Ω_y denote open subsets of \mathbb{R}^2 and \mathbb{R} , respectively, $\mathbb{R}_T \subset \mathbb{R}$ represents
 24 an open time interval covering the time required for the measuring process, $a \in$
 25 $C^\infty(\mathbb{R}_T \times \Omega_y \times \Omega_x)$ is a weight function and $H : \mathbb{R}_T \times \mathbb{R}^2 \rightarrow \mathbb{R}$ characterizes the
 26 manifold we are integrating over.

With this observation model, we can formulate the associated inverse problem: Determine h from measured data

$$g(t, y) = \mathcal{A}h(t, y), \quad (t, y) \in \mathbb{R}_T \times \Omega_y. \quad (3)$$

1 The component t of the data variable expresses the time-dependency of the data
 2 collection process. The searched-for quantity h itself, however, is independent of
 3 time, i.e. (3) corresponds to a *static* image reconstruction problem. We refer to
 4 equation (3) also as *static inverse problem*.

2.1. The mathematical model of dynamic imaging. Now, we consider the dynamic case, i.e. the investigated object changes during collection of the data and is therefore characterized by a time-dependent function $f : \mathbb{R}_T \times \mathbb{R}^2 \rightarrow \mathbb{R}$. For a fixed time, we abbreviate $f_t := f(t, \cdot)$, i.e. f_t represents the state of the object at time instance t . Then, the inverse problem of the dynamic scenario reads

$$\mathcal{A}^{\text{dyn}} f(t, y) = g(t, y) \quad (4)$$

5 with the dynamic operator $\mathcal{A}^{\text{dyn}} f(t, y) := \mathcal{A}f_t(t, y)$. In particular, only measure-
 6 ments $g(t, \cdot)$ for a single time instance encode information about the state f_t , which
 7 is typically not sufficient to fully recover f_t . In CT, only line integrals in one partic-
 8 ular direction would be available for the reconstruction of f_t , which is well known
 9 to be insufficient. Thus, additional information about the dynamic behavior need
 10 to be incorporated in order to solve dynamic inverse problems.

11 The dynamic behaviour of the object can be considered to be due to particles
 12 which change position in a fixed coordinate system of \mathbb{R}^2 . This physical interpre-
 13 tation of object movement can then be incorporated into a mathematical model
 14 $\Phi : \mathbb{R}_T \times \mathbb{R}^2 \rightarrow \mathbb{R}^2$, where $\Phi(0, x) = x$, i.e. we consider f_0 as reference state,
 15 and $\Phi(t, x)$ denotes the position at time t of the particle initially at x . For fixed
 16 $t \in \mathbb{R}_T$, we write $\Phi_t x := \Phi(t, x)$ to simplify the notation. Motivated by medical
 17 applications, where no particle is lost or added and two particles cannot move to
 18 the same position at the same time, Φ_t is assumed to be a diffeomorphism for all
 19 $t \in \mathbb{R}_T$. Thus, a particle $x \in \mathbb{R}^2$ at time t is at position $\Phi_t^{-1}x$ in the reference state,
 20 see Figure 1. A description of this motion model can also be found, for instance, in
 21 [16, 26, 27].

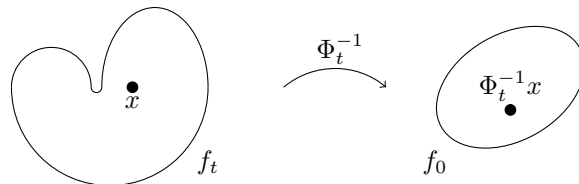


FIGURE 1. The mapping Φ_t^{-1} correlates the state f_t at time t to the reference state f_0 at the initial time.

Using this motion model and the initial state function f_0 , we find the state of the object at time instance t to be

$$f(t, x) = f_0(\Phi_t^{-1}x) |\det D\Phi_t^{-1}x| \quad (5)$$

22 by taking into account that mass shall be preserved.

23

Inserting the property (5) in the definition of the dynamic forward operator \mathcal{A}^{dyn} , we obtain an operator \mathcal{A}_Φ for the initial state function, namely

$$\mathcal{A}_\Phi f_0(t, y) := \mathcal{A}(|\det D\Phi_t^{-1}(\cdot)|(f_0 \circ \Phi_t^{-1}))(t, y). \quad (6)$$

1 **Remark 1.** In our previous work [16, 17, 21], we considered the intensity preserving
2 model

$$f(t, x) = f_0(\Phi_t^{-1}x),$$

3 i.e. each particle keeps its initial intensity over time. Although this does not alter
4 the nature of our reconstruction algorithm, we insist here on the mass preserving
5 case to be consistent with the conservation laws employed in Section 3 for the
6 purpose of motion estimation and clinical applications. The mass preserving model
7 is also considered, for instance, in [26, 27].

8 For a theoretical analysis, the motion model Φ is typically assumed to satisfy the
9 following additional conditions, cf. [38, 9, 21, 19]:

10 • The map

$$x \mapsto \begin{pmatrix} H(t, \Phi_t x) \\ D_t H(t, \Phi_t x) \end{pmatrix} \quad (7)$$

11 is one-to-one for each t .

12 • It holds

$$\det \begin{pmatrix} D_x H(t, \Phi_t x) \\ D_x D_t H(t, \Phi_t x) \end{pmatrix} \neq 0 \quad (8)$$

13 for all $x \in \mathbb{R}^2$ and all $t \in \mathbb{R}_T$.

14 Basically, these properties ensure that the object's motion does not result in trivial
15 sampling schemes for f_0 . A detailed interpretation of these conditions can be found,
16 for instance, in [21].

If the deformation fields Φ_t are known, the dynamic inverse problem (4) reduces to determining f_0 from the equation

$$\mathcal{A}_\Phi f_0 = g. \quad (9)$$

17 In [18, 16, 26], efficient algorithms have been developed to solve this task. The
18 underlying strategy proposed in [18] is summarized in the following, before we
19 introduce our PDE-based approach to determine the deformation fields Φ_t in Section
20 3 and combine both strategies to solve (9) when Φ_t are unknown.

21 **2.2. Motion compensation algorithms.** Throughout this section, we assume
22 the motion Φ to be known and focus on solving (9). Under suitable assumptions on
23 the phase function H , the linear integral operator \mathcal{A} from the underlying static case
24 belongs to the class of *Fourier integral operators*. To define this type of operators,
25 we first introduce the concepts of amplitude and phase function.

26 **Definition 2.1.**

27 • Let $\Lambda \in C^\infty(\mathbb{R}_T \times \Omega_y \times \Omega_x \times \mathbb{R} \setminus \{0\})$ be a real-valued function with the
28 following properties:

- 29
- 30 1. Λ is positive homogeneous of degree 1 in σ , i.e. $\Lambda(t, y, x, r\sigma) =$
31 $r\Lambda(t, y, x, \sigma)$ for every $r > 0$,
 - 32 2. both $(\partial_{(t,y)}\Lambda, \partial_\sigma\Lambda)$ and $(\partial_x\Lambda, \partial_\sigma\Lambda)$ do not vanish for all $(t, y, x, \sigma) \in \mathbb{R}_T \times$
33 $\Omega_y \times \Omega_x \times \mathbb{R} \setminus \{0\}$,
 3. it holds $\partial_{(t,y,x)} \left(\frac{\partial\Lambda}{\partial\sigma} \right) \neq 0$ on the zero set

$$\Sigma_\Lambda = \{(t, y, x, \sigma) \in \mathbb{R}_T \times \Omega_y \times \Omega_x \times \mathbb{R} \setminus \{0\} : \partial_\sigma\Lambda = 0\}.$$

1 Then, Λ is called a *non-degenerate phase function*.

- Let $a \in C^\infty(\mathbb{R}_T \times \Omega_y \times \Omega_x \times \mathbb{R})$ satisfy the following property:
For every compact set $K \subset \mathbb{R}_T \times \Omega_y \times \Omega_x$ and for every $M \in \mathbb{N}$, there exists a $C = C(K, M) \in \mathbb{R}$ such that

$$\left| \frac{\partial^{n_1}}{\partial t^{n_1}} \frac{\partial^{n_2}}{\partial y^{n_2}} \frac{\partial^{n_3}}{\partial x_1^{n_3}} \frac{\partial^{n_4}}{\partial x_2^{n_4}} \frac{\partial^m}{\partial \sigma^m} a(t, y, x, \sigma) \right| \leq C(1 + |\sigma|)^{k-m}$$

2 for $n_1 + n_2 + n_3 + n_4 \leq M$, $m \leq M$, for all $(t, y, x) \in K$ and for all $\sigma \in \mathbb{R}$.

3 Then a is called an *amplitude* (of order k).

- Let Λ denote a non-degenerate phase function and let a be an amplitude (of order k). Then, the operator \mathcal{T} defined by

$$\mathcal{T}u(t, y) = \int u(x)a(t, y, x, \sigma)e^{i\Lambda(t, y, x, \sigma)} dx d\sigma, \quad (t, y) \in \mathbb{R}_T \times \Omega_y$$

4 is called a *Fourier integral operator* (FIO) (of order $k - 1/2$).

5 For more details and a more general definition see [22, 44].

6
7 In [18, 19], it was shown that under suitable smoothness conditions on Φ , the
8 dynamic operator \mathcal{A}_Φ inherits the FIO property from its static counterpart \mathcal{A} .

9 **Theorem 2.2.** *Let $\Phi \in C^\infty(\mathbb{R}_T \times \mathbb{R}^2)$ and let Φ_t be a diffeomorphism for every
10 $t \in \mathbb{R}_T$. If the static operator \mathcal{A} from (2) is an FIO, the respective dynamic operator
11 \mathcal{A}_Φ from (6) is an FIO as well.*

12 Fourier integral operators have specific properties that can be used to design
13 efficient motion compensation strategies: They encode characteristic features of the
14 object - the so-called *singularities* - in precise and well-understood ways.

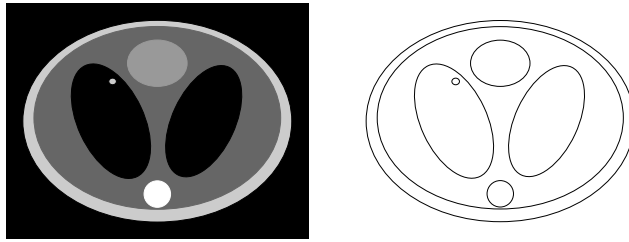


FIGURE 2. Initial state f_0 of a phantom (left) and its singularities (right).

15 Formally, singularities of a (generalized) function h correspond to the elements
16 of the *singular support* $\text{ssupp}(h)$, which denotes the complement of the largest open
17 set on which h is smooth. In imaging applications, where the searched-for quantity
18 is typically piecewise constant (each value characterizing a particular material), the
19 singularities correspond to the contours of h , see Figure 2.

The method for motion compensation from [18] is motivated by results on microlocal analysis, which address - among others - the question which singularities can be stably recovered from the data. The main idea is to use reconstruction operators of the form

$$\mathcal{L}_\Phi = \mathcal{B}_\Phi \mathcal{P} \tag{10}$$

1 on the data $g = \mathcal{A}_\Phi f_0$ with \mathcal{P} a *pseudodifferential operator* (typically acting on the
 2 spatial data variable y) and a *backprojection operator* \mathcal{B}_Φ which incorporates the
 3 information on the dynamic behavior.

Definition 2.3. a) An operator of the form

$$\mathcal{P}g(t, s) = \int_{\mathbb{R}} \int_{\mathbb{R}} e^{i\sigma(s-y)} p(s, y, \sigma) g(t, y) dy d\sigma$$

4 with $|\sigma| \leq 1$ and amplitude p which is locally integrable for s, y in any compact
 5 set K is called *pseudodifferential operator (PSIDO)* (acting on the spatial data
 6 variable y).

b) The operator

$$\mathcal{B}_\Phi g(x) = \int_{\mathbb{R}_T} b(t, x) g(t, H(t, \Phi_t x)) dt, \quad x \in \mathbb{R}^2,$$

7 where $b(t, x)$ is a positive C^∞ -weight function on $\mathbb{R}_T \times \mathbb{R}^2$, is called *backpro-*
 8 *jection operator* associated to \mathcal{A}_Φ .

9 With these representations of \mathcal{B}_Φ and \mathcal{P} , the operator \mathcal{L}_Φ from (10) reads

$$\mathcal{L}_\Phi g(x) = \int_{\mathbb{R}_T} \int_{\mathbb{R}} \int_{\mathbb{R}} b(t, x) p(H(t, \Phi_t x), y, \sigma) g(t, y) e^{i\sigma(H(t, \Phi_t x) - y)} dy d\sigma dt. \quad (11)$$

10 **Remark 2.** a) Pseudodifferential operators constitute a special case of an FIO.

11 A more general definition than the one given above can be found, for instance,
 12 in [30].

13 b) If we choose the weight $b(t, x) = a(t, H(t, \Phi_t), \Phi_t x)$ with the amplitude a of
 14 the underlying static operator \mathcal{A} , the respective backprojection operator \mathcal{B}_Φ
 15 corresponds to the dual operator of \mathcal{A}_Φ .

16 The following result forms the basis to our motion compensation method.

17 **Theorem 2.4.** Let $\Phi \in C^\infty(\mathbb{R}_T \times \mathbb{R}^2)$ and let $\Phi_t, t \in \mathbb{R}_T$ be diffeomorphisms that
 18 satisfy the conditions (7) and (8). Further, let $\mathcal{L}_\Phi = \mathcal{B}_\Phi \mathcal{P}$ be well-defined. Then,
 19 \mathcal{L}_Φ preserves the singularities of f_0 which are ascertained in the measured data.

20 *Proof.* The statement follows directly from Theorem 13 in [19]. \square

21 **Interpretation:** Applying a reconstruction operator \mathcal{L}_Φ of type (10) provides
 22 an image showing the singularities of f_0 correctly, which are encoded by the dy-
 23 namic data. In particular, no motion artefacts arise. Thus, the described approach
 24 provides in fact a motion compensation strategy. In particular, it can be easily
 25 implemented and the computational effort is comparable to the one of static recon-
 26 struction algorithms of type *filtered backprojection*. If an inversion formula of type
 27 $u = \mathcal{A}^* \mathcal{P}^{stat} \mathcal{A} u$ with a PSIDO \mathcal{P}^{stat} is known for the static case, then choosing
 28 the PSIDO $\mathcal{P} = \mathcal{P}^{stat}$ for the motion compensation strategy provides even a good
 29 approximation to the exact density values of f_0 [18]. In computerized tomography,
 30 such an inversion formula is known with \mathcal{P}^{stat} being the *Riesz potential* [35].

31

32 **Remark 3.** Although the ascertained singularities of f_0 are correctly reconstructed
 33 by \mathcal{L}_Φ , some additional artefacts might occur if the motion is non-periodic. This
 34 has been studied in detail for computerized tomography in [21] and for a more
 35 general class of imaging problems in [19]. These artefacts would be caused by
 1 singularities encoded at beginning and end of the scanning and would spread along

2 the respective integration curve. Nevertheless, this is an intrinsic property due to the
 3 nature of the dynamic problem and therefore does not impose a major restriction
 4 to our reconstruction approach. In particular, for periodic motion as in medical
 5 applications, such as respiratory motion, the data acquisition protocol could be
 6 adjusted to the breathing cycle to avoid this issue.

7 Since inverse problems are typically ill-posed, a regularization is required to de-
 8 termine $\mathcal{L}_\Phi g$ stably from the measured data $g = \mathcal{A}_\Phi f_0$. For our considered class
 9 of imaging problems, the ill-posedness is typically revealed by the growth of the
 10 symbol p in terms of σ . For instance, the amplitude of the Riesz potential arising
 11 in computerized tomography corresponds to $p(s, y, \sigma) = p(\sigma) = |\sigma|$, thus, amplify-
 12 ing the high frequencies of the data g . The inversion process can be stabilized by
 13 introducing a smooth low-pass filter e^γ , i.e. by considering

$$\mathcal{L}_\Phi^\gamma g(x) = \int_{\mathbb{R}_T} \int_{\mathbb{R}} \int_{\mathbb{R}} b(t, x) p(H(t, \Phi_t x), y, \sigma) e^\gamma(\sigma) g(t, y) e^{i\sigma(H(t, \Phi_t x) - y)} dy d\sigma dt \quad (12)$$

14 with $\gamma > 0$ instead of (11), see [18] for more details.

15 **2.3. Reconstruction operator in dynamic CT.** Since we will evaluate our mo-
 16 tion estimation strategy in Section 5 at the example of computerized tomography,
 17 we want to state the respective motion compensation algorithm for this application
 18 explicitly.

As introduced in the beginning of this section, the mathematical model operator \mathcal{A} of the static case corresponds to the classical Radon transform \mathcal{R} , see (1), which is an FIO with amplitude $a(t, y, x) = (2\pi)^{-1/2}$ and phase function $\Lambda(t, y, x, \sigma) = \sigma(y - H(t, x))$, where $H(t, x) = x^T \theta(t)$ [30]. Thus, the associated dynamic backprojection operator \mathcal{B}_Φ with weight $b(t, x) = a(t, H(t, \Phi_t), \Phi_t x) = (2\pi)^{-1/2}$ reads

$$\mathcal{B}_\Phi g(x) = (2\pi)^{-1/2} \int_{\mathbb{R}_T} g(t, (\Phi_t x)^T \theta(t)) dt.$$

Choosing as PSIDO the Riesz potential with amplitude $p(s, y, \sigma) = |\sigma|$ and a low-pass filter e^γ , for instance the Gaussian, we obtain the dynamic reconstruction operator

$$\mathcal{L}_\Phi^\gamma g(x) = (2\pi)^{-1/2} \int_{\mathbb{R}_T} \int_{\mathbb{R}} \int_{\mathbb{R}} |\sigma| e^\gamma(\sigma) g(t, y) e^{i\sigma((\Phi_t x)^T \theta(t) - y)} dy d\sigma dt, \quad \gamma > 0,$$

19 which can be implemented in form of a *filtered backprojection* type algorithm, see
 20 [17].

21 **3. Linear elastics.** In this section and the following one, we will treat the task
 22 of motion estimation. While, for a global deformation, the dynamic behavior of
 23 the boundary can be observed externally, the deformation in the interior is a priori
 24 unknown. Since many dynamic processes can be mathematically described in terms
 25 of a partial differential equation (PDE), we propose to determine the deformation
 26 fields Φ_t by finding the solution of an appropriate PDE with suitable given initial
 27 and boundary data.

28
 29 Since the deformation fields $\Phi_t, t \in \mathbb{R}_T$ describe the mapping from the initial/reference
 30 state to the current position, we choose the Lagrangian description for the PDE.

1 Let $\Omega_x \subset \mathbb{R}^2$ denote the initial domain, i.e. Ω_x corresponds to the support of the
 2 initial state f_0 , and consequently, we choose Ω_x to be the reference configuration.

3 We require that $\Phi_t, t \in \mathbb{R}_T$ preserves its orientation meaning that $\det D\Phi(t, x) >$
 4 0 for all $(t, x) \in \mathbb{R}_T \times \Omega_x$. Especially in medical applications, this assumption is
 5 sensible since it also states that the local ratio of the current and the initial volume
 6 never vanishes. [1]

7
 8 The following definition links the current and the initial position.

9 **Definition 3.1.** The difference between the current and the initial position is called
 10 displacement $u(t, x) = \Phi(t, x) - x$ for all $(t, x) \in \mathbb{R}_T \times \Omega_x$.

11 Our investigations are driven by medical applications. Having the cross section
 12 of a thorax in mind, we consider two spatial dimensions, which is reasonable under a
 13 plane strain assumption. The properties of respiratory motion shall then be reflected
 14 by adequate equations. Due to its periodic behavior, it is clear that occurring
 15 stresses do not cause any yielding. So we assume a linear relationship between
 16 stresses and strain which results in linear elasticity. In future work, we plan to
 17 consider more general stress-strain laws.

We consider this paper a proof-of-concept. Thus we insert Hooke's law in the
 general equation of conservation of momentum and arrive at the Navier-Cauchy
 equations in two spatial dimensions for $(t, x) \in \mathbb{R}_T \times \Omega_x$, see for reference [43]:

$$\hat{\rho} \frac{\partial^2 u_k}{\partial t^2} = \hat{v}_k + \mu \left(\frac{\partial^2 u_k}{\partial x_1^2} + \frac{\partial^2 u_k}{\partial x_2^2} \right) + (\lambda + \mu) \frac{\partial}{\partial x_k} \left(\frac{\partial u_1}{\partial x_1} + \frac{\partial u_2}{\partial x_2} \right) \quad \text{for } k = 1, 2. \tag{13}$$

18 These are two linear PDEs for the two unknown components u_1, u_2 of the dis-
 19 placement u with the following parameters:

- 20 • The density $\hat{\rho} = \rho(t, x) \det D\Phi(t, x)$ equals the initial density distribution
 21 $\hat{\rho} = \hat{\rho}(x) = \rho(0, x)$ due to the conservation of mass.
- 22 • The external volume forces are denoted by $\hat{v} = v(t, x) \det D\Phi(t, x)$, where
 23 $v : \mathbb{R}_T \times \Omega_x \rightarrow \mathbb{R}^2$ describes the volume force density.
- 24 • The Lamé-coefficients λ and μ specify the behavior of the material.

For a fully determined problem, we need the displacements at time $t = 0$ and
 their time derivatives as initial data

$$u(0, x) = \vartheta^0(x) \quad \text{and} \quad \frac{\partial}{\partial t} u(0, x) = \vartheta^1(x),$$

with some given $\vartheta^0, \vartheta^1 : \Omega_x \rightarrow \mathbb{R}^2$.

Also the behavior of the boundary needs to be known, more precisely a function
 $\psi : \mathbb{R}_T \times \Omega_x \rightarrow \mathbb{R}^2$ prescribing the evolution of the displacements on the boundary
 of the domain $\Gamma = \partial\Omega_x$:

$$u(t, x) = \psi(t, x) \quad \text{for } (t, x) \in \mathbb{R}_T \times \Gamma.$$

25 Solving the PDE we have introduced with given initial and boundary conditions
 26 corresponds to determining the displacement u , respectively the deformation Φ in
 27 the interior of the object from observations of the dynamic behavior of the object's
 28 boundary. This way we model the movement in the object's interior, which provides
 1 exactly the information about the motion needed for our motion compensation al-
 2 gorithm.

3

4 Under some regularity assumptions, existence and uniqueness of the solutions of
 5 the Navier-Cauchy equation (13) can be proven. If the initial data is C^∞ , solutions
 6 for the initial value problem stay C^∞ , cf. [23]. Also for the initial-boundary value
 7 problem, there are existence and uniqueness results, cf. [7]. For appropriate bound-
 8 ary data ψ , regularity of the solutions does not get lost, and it can be shown that
 9 the solutions are diffeomorphisms, cf. [10]. In our numerical experiments in Section
 10 5, the initial and boundary data is chosen so that the application of the motion
 11 compensation algorithm goes through.

12

13 In the following, we quickly discuss suitable initial and boundary data regarding
 14 our application in dynamic imaging. As mentioned before, a global motion can be
 15 observed externally, thus, we make the reasonable assumption that the boundary
 16 data $\psi(t, x)$, $(t, x) \in \mathbb{R}_T \times \Gamma$ are given. However, in practice, only discrete boundary
 17 data $\psi(t_n, x_{i,j})$, $n = 1, \dots, N$, $i = 1, \dots, I$, $j = 1, \dots, J$, $N, I, J \in \mathbb{N}$ will be available
 18 which might be even sparse with respect to the spatial component (i.e. I, J might
 19 be small) or corrupted by noise. This will be addressed in our numerical study in
 20 Section 5.

21 Since we are overall interested in a reconstruction of the initial state of the object
 22 and since we start with an undeformed configuration, the initial displacement data
 23 ϑ^0 and ϑ^1 will be set to zero.

24 **Remark 4.** According to (13), the Navier-Cauchy contains the initial density dis-
 25 tribution $\hat{\rho}$ as parameter which is strongly linked to the quantity f_0 we would like
 26 to determine by our imaging modality (in particular, they share the same singular-
 27 ities). If we knew this parameter $\hat{\rho}$, we would already have full knowledge about
 28 the interior structure of the studied specimen. Thus, we cannot assume to know $\hat{\rho}$.
 29 Formally, we could formulate a joint motion estimation and image reconstruction
 30 approach, where we identify the parameter $\hat{\rho}$ of the PDE using the measurements
 31 from our imaging modality. However, to simplify the task for our proof-of-concept
 32 study, we propose another approach. In order to decouple the tasks of motion esti-
 33 mation via the Navier-Cauchy equation and dynamic image reconstruction, we use
 34 for the solution of the PDE a simplified prior instead of the exact density distribu-
 35 tion $\hat{\rho}$. This is discussed in more detail in Section 5.

36 **4. Numerical solution of the Navier-Cauchy equation.** We divide the given
 37 time period $t \in \mathbb{R}_T$ into equidistant intervals and call the time steps $t_n = n \cdot \Delta t$. We
 38 choose a Cartesian grid (not necessarily uniform) so that the discrete boundary lies
 39 on the continuous boundary, see Figure 4. Using central finite differences of second
 40 order for the discretization of the Navier-Cauchy equation (13), we obtain an explicit
 41 numerical scheme. We have chosen finite difference for our proof-of-concept study.
 42 For future studies, we plan to use a more elaborated numerical method.

We denote $x_{i,j} = ((x_1)_i, (x_2)_j) = (x_i, y_j)$, $(u_k)_{i,j}^n = u_k(t_n, x_{i,j})$ for $k = 1, 2$,
 $\rho_{i,j}^0 = \hat{\rho}(x_{i,j})$, $\hat{v}_{i,j}^n = \hat{v}(t_n, x_{i,j})$, $\Delta x_i = x_{i+1} - x_i$ and $\Delta y_j = y_{j+1} - y_j$. Then the

scheme reads exemplary for the first component $k = 1$

$$\begin{aligned}
 (u_1)_{i,j}^{n+1} &= \frac{\Delta t^2}{\rho_{i,j}^0} \hat{v}_{i,j}^n - (u_1)_{i,j}^{n-1} + 2 \left[1 - \frac{2\Delta t^2}{\rho_{i,j}^0} \left(\frac{\mu}{\Delta y_j^2 + \Delta y_{j-1}^2} + \frac{\lambda + 2\mu}{\Delta x_i^2 + \Delta x_{i-1}^2} \right) \right] (u_1)_{i,j}^n \\
 &+ \frac{\Delta t^2}{\rho_{i,j}^0} \frac{2(\lambda + 2\mu)}{\Delta x_i^2 + \Delta x_{i-1}^2} \left[\left(1 - \frac{\Delta x_i - \Delta x_{i-1}}{\Delta x_i + \Delta x_{i-1}} \right) (u_1)_{i+1,j}^n + \left(1 + \frac{\Delta x_i - \Delta x_{i-1}}{\Delta x_i + \Delta x_{i-1}} \right) (u_1)_{i-1,j}^n \right] \\
 &+ \frac{\Delta t^2}{\rho_{i,j}^0} \frac{2\mu}{\Delta y_j^2 + \Delta y_{j-1}^2} \left[\left(1 - \frac{\Delta y_j - \Delta y_{j-1}}{\Delta y_j + \Delta y_{j-1}} \right) (u_1)_{i,j+1}^n + \left(1 + \frac{\Delta y_j - \Delta y_{j-1}}{\Delta y_j + \Delta y_{j-1}} \right) (u_1)_{i,j-1}^n \right] \\
 &+ \frac{\Delta t^2}{\rho_{i,j}^0} \frac{\lambda + \mu}{(\Delta x_i + \Delta x_{i-1})(\Delta y_j + \Delta y_{j-1})} \left((u_2)_{i+1,j+1}^n - (u_2)_{i-1,j+1}^n - (u_2)_{i+1,j-1}^n + (u_2)_{i-1,j-1}^n \right).
 \end{aligned}$$

1 The corresponding stencil is illustrated in Figure 3.

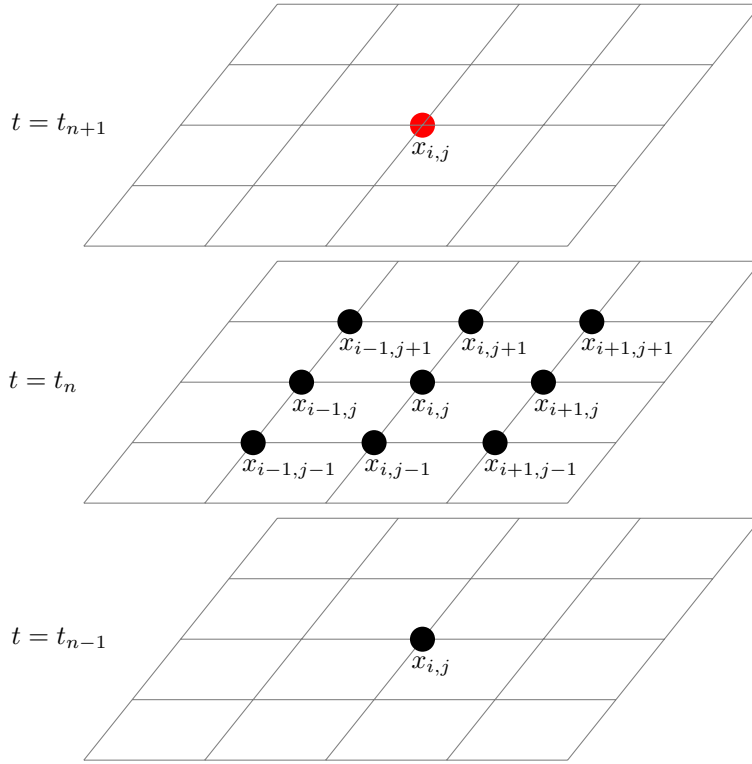


FIGURE 3. We illustrate the stencil for our numerical scheme. For the update of the values at node $x_{i,j}$ from $t_n \rightarrow t_{n+1}$, we have to provide information about the values at the other marked nodes.

For the first time step, the (discrete) initial condition needs to be inserted

$$(u_k)_{i,j}^{-1} = (u_k)_{i,j}^1 - 2\Delta t \vartheta^1(x_{i,j}) \quad \text{for } k = 1, 2.$$

2 The stencil for the spatial discretization has nine nodes. Since we are inspired by
 3 medical applications and a thorax is a possible specimen to be studied, we might
 4 deal with curved domains. For curved domains at the boundary, for the update
 5 scheme there is a node, which is not available to the stencil, see Figure 4. Hence,
 6 we need to use an interpolation method.

For reasons of stability, we want to maintain the stencil. We call the missing node a ghost node that needs to have a value assigned to it, and we denote h the

quantities given at every node. The indices of the nodes are given in Figure 4. A second-order approach is the following one for the components $k = 1, 2$:

$$(h_k)_{\text{ghost}} = (h_k)_0 + \frac{(h_k)_{\text{aux}} - (h_k)_0}{(x_k)_{\text{aux}} - (x_k)_0} ((x_k)_{\text{ghost}} - (x_k)_0)$$

where the auxiliary node on the continuous boundary is approximated by

$$x_{\text{aux}} = \frac{1}{2} ((x_1)_1 + (x_1)_0), \quad y_{\text{aux}} = \frac{1}{2} ((x_2)_2 + (x_2)_0) \quad \text{and}$$

$$(h_k)_{\text{aux}} = \frac{1}{2} ((h_k)_1 + (h_k)_2).$$

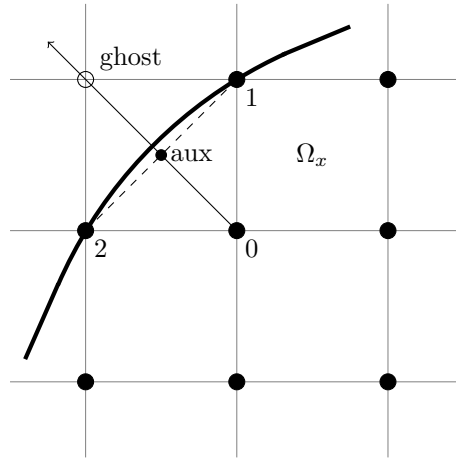


FIGURE 4. Illustration of the boundary: The nodes 1 and 2 lie directly on the continuous boundary, and their behaviour is prescribed by the Dirichlet data ψ . For the node 0, the stencil for the update scheme only can be applied with the help of an interpolation since the values of the ghost node are not available. The average of the values of the nodes 1 and 2 are used to create an auxiliary node which corresponds to a slightly ‘shifted’ boundary.

1

We use the CFL condition

$$\frac{\nu_x \Delta t}{\Delta x} + \frac{\nu_y \Delta t}{\Delta y} \leq 1,$$

- 2 where $\Delta x := \min \Delta x_i$ and $\Delta y := \min \Delta y_j$, in order to determine a suitable time
 3 step Δt . The maximal propagation speeds are bounded from above by $\nu_x, \nu_y \leq$
 4 $\sqrt{(\lambda + 2\mu)/\rho}$ with $\rho := \min \rho_{i,j}^0 > 0$.

5. Application in motion compensation. We evaluate the motion estimation approach on simulated CT data. For this purpose, we consider a thorax phantom representing a cross-section of a chest, see Figure 5 left. Following from [11], its respiratory motion is modelled by an affine deformation, more precisely by

$$\Phi(t, x) = \begin{pmatrix} s(t)^{-1} & 0 \\ 0 & s(t) \end{pmatrix} \left(x - \begin{pmatrix} 0.44 \cdot (s(t) - 1) \\ 0 \end{pmatrix} \right)$$

1 with $s(t) = 0.05 \cdot \cos(0.04 \cdot t) + 0.95$. The deformation during one breathing cycle
 2 is illustrated in the sequence of pictures in Figure 5.

3

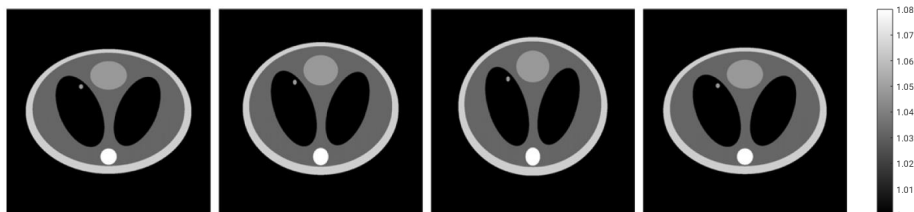


FIGURE 5. Cross-section of the numerical phantom during one cycling breath.

4 The Radon data of this dynamic object are computed analytically for 660 source
 5 positions, uniformly distributed over the upper half sphere, and 451 discrete detec-
 6 tor points uniformly distributed over $[-1, 1]$ (since the support of the phantom is
 7 contained in the unit disk at all time instances). Our reconstructions and - later on
 8 - all simulations of the PDE are run on a 257×257 grid.

9

10 If one does not take into account that the object was moving during data acquisi-
 11 tion and applies a static reconstruction algorithm to the dynamic data, an image of
 12 poor quality with motion artefacts such as blurring, streaking etc. is obtained, see
 13 Figure 6(b). This motivates the need for motion compensation and hence motion
 14 estimation strategies.

15 As motion compensation algorithm, we use the strategy specified in Section 2.3
 16 with the Gaussian function as low-pass filter. The result of this algorithm with exact
 17 motion information Φ is shown in Figure 6(c). We observe that all components are
 18 indeed correctly reconstructed without motion artefacts, i.e. the motion is well
 19 compensated for, and in accordance to [18], we obtain a good approximation to
 20 the original initial state, cf. Figure 6(a). However, in practice, the exact motion
 21 information is typically unknown.

22 Thus, our goal is now to evaluate our proposed motion estimation strategy, i.e.
 23 the (discrete) deformation fields Φ_t are computed by solving the Navier-Cauchy
 24 equation with available initial and boundary data. First, we discuss the initial data
 25 corresponding to the initial density distribution $\hat{\rho}$. As discussed in Remark 4, this
 26 initial parameter is strongly linked to the searched-for initial state function f_0 which
 27 is why we propose to use a simplified prior instead. The one used for our simulation
 28 is shown in Figure 7. This prior only distinguishes between spine and soft tissue,
 29 where the respective values are initialized with standard values $\hat{\rho} = 1.85 \cdot 10^3 \text{ kg/m}^3$
 30 for the spine and $\hat{\rho} = 1.05 \cdot 10^3 \text{ kg/m}^3$ for the rest. This is indeed a reasonable
 31 prior in practice since the only component considered in the interior - the spine
 32 - typically does not move, so it can be extracted from a static reconstruction, cf.
 33 Figure 6(b). This prior can optionally be improved by an iteration between the
 34 motion estimation with given $\hat{\rho}$ and image reconstructions, which then update $\hat{\rho}$
 35 again.

36 Finding realistic values for the Lamé-coefficients of human tissue is a research
 37 topic by itself. It is hard to quantify them and they differ depending on the study

1 [47]. We assume a uniform motion behavior of all (soft) tissues and restrict our-
 2 selves to one set of values for the whole thorax. The coefficients are averaged to
 3 $\lambda = 3.46$ kPa and $\mu = 1.48$ kPa.
 4

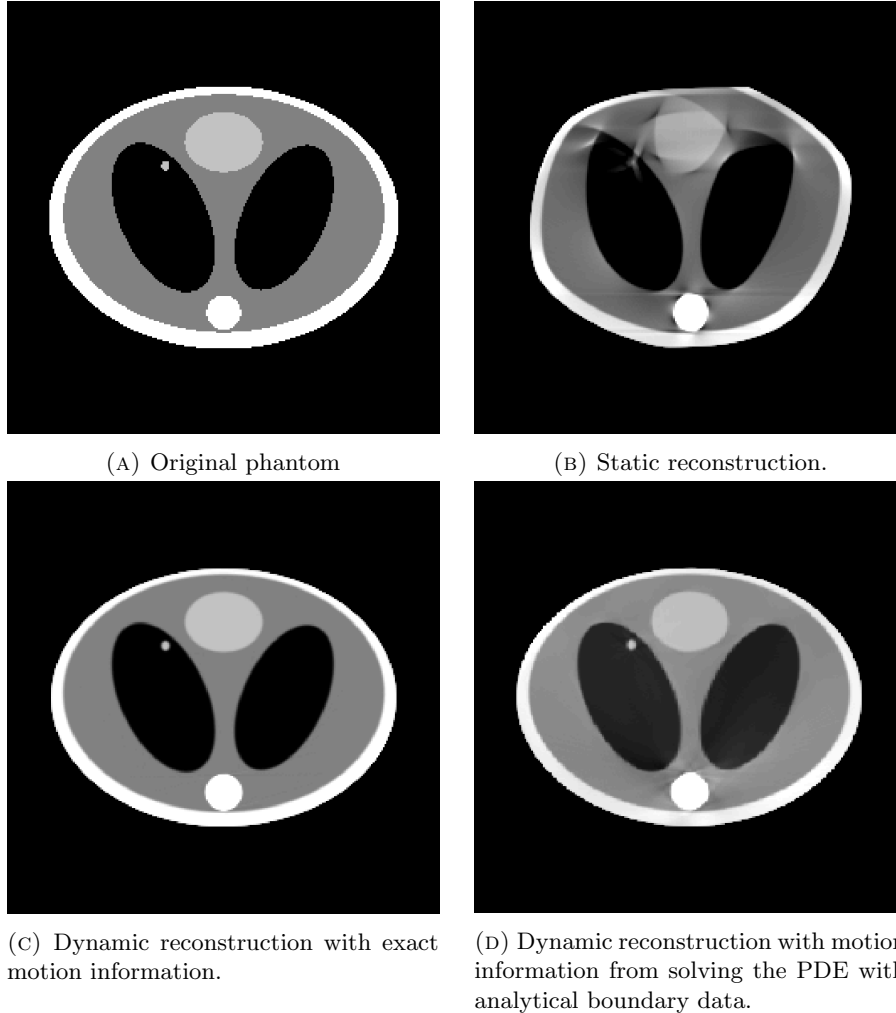


FIGURE 6. Static and dynamic reconstruction results of the initial state function.

5 Regarding the boundary data, we test several configurations. First, we use the
 6 exact analytical positions of the boundary. Then, solving the respective PDE as
 7 described in Section 4 and incorporating its solution as motion information in our
 8 dynamic reconstruction algorithm provides the reconstruction result shown in Fig-
 9 ure 6(d). The motion of the phantom is well compensated for and the small tumour
 10 is clearly visible. This shows that determining deformation fields by solving the
 11 Navier-Cauchy equation constitutes a valuable motion estimation strategy.

12 In practice, the boundary positions might be determined by attaching markers
 13 at the surface of the object. If these positions are determined by measurements,

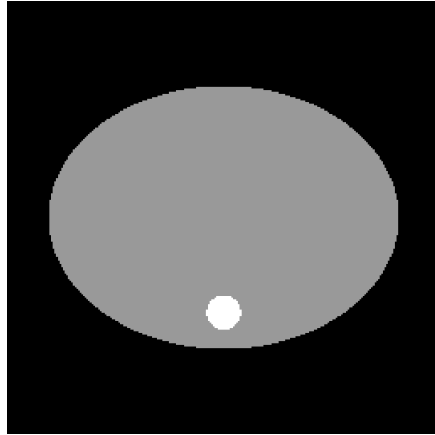
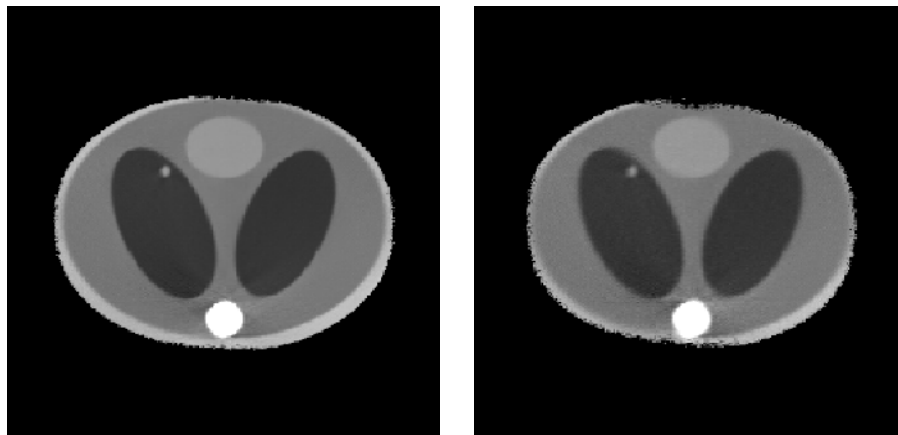


FIGURE 7. Initial density distribution used for solving the Navier-Cauchy equation.

1 they will be subject to small measurement errors. Thus, in order to test stability
 2 with respect to the boundary data, we next add a sample of noise to the (ana-
 3 lytical) boundary positions. The noise is generated as normal distribution around
 4 0 with standard deviation 0.1 and 0.25, respectively. In Figure 8 we see that the
 5 reconstruction near the boundary is affected. More precisely, due to the inexact
 6 boundary positions, the boundary in the reconstruction appears fuzzy. However,
 7 the motion in the interior of the phantom is still well compensated for. All interior
 8 components, which correspond to the relevant searched-for information, including
 9 the small tumour, are still clearly recognizable, in particular in comparison to the
 10 static reconstruction, cf. Figure 6(b).

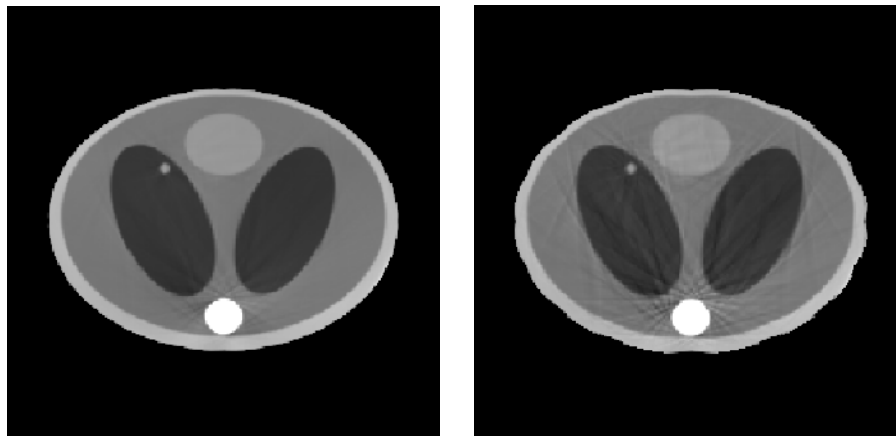


(A) Result for noisy boundary data with standard deviation 0.1.

(B) Result for noisy boundary data with standard deviation 0.25.

FIGURE 8. Dynamic reconstruction with motion information from solving the PDE with noisy boundary data.

1 Further, we test the performance of the method if only a few discrete boundary
 2 positions are given. The motivation behind this experiment is that, in practice,
 3 only a limited number of markers can be attached to the surface of the object. To
 4 this end, we prescribe only 32 (and 16, respectively) grid nodes on the boundary.
 5 Between these nodes, we apply a linear interpolation. The results are displayed in
 6 Figure 9. We obtain some artefacts since the round shape of the thorax is replaced
 7 by a polygon due to the interpolation. However, as in the case of noisy boundary
 8 data, the deformation fields obtained by solving the PDE still provide sufficient
 9 information on the motion to compensate for it in the interior and to provide an
 10 image showing clearly all inner components including the small tumour.



(A) Result for 32 prescribed boundary nodes.

(B) Result for 16 prescribed boundary nodes.

FIGURE 9. Dynamic reconstruction results with motion information from solving the PDE with only a small number of boundary nodes.

11 **6. Conclusions and Outlook.** This article provides a proof-of-concept for a motion
 12 estimation strategy in dynamic imaging, where the Navier-Cauchy equation
 13 serves as a mathematical model for small elastic deformations. To this end, we
 14 decoupled the tasks of motion estimation and image reconstruction, i.e. the Navier-
 15 Cauchy equation is solved prior to the reconstruction step using suitable and realistic
 16 initial and boundary data. Then the calculated deformation fields are incorporated
 17 into an analytic dynamic reconstruction algorithm. Our numerical results on a
 18 thorax phantom undergoing respiratory motion illustrate that this approach can
 19 significantly reduce motion artefacts in the respective images. In particular, we
 20 discussed available boundary data and illustrated their affect on the reconstruction
 21 result.

22 In future work, a more realistic biomechanical material law than Hooke's law
 23 will be considered. More elaborated numerical schemes will then be implemented
 24 for more specific studies. A worthwhile approach might be to minimize the distance
 25 between observed and simulated displacements in combination with solving
 26 an initial boundary value problem.

1 So far, we have decoupled the suggested motion estimation and compensation
 2 approach: For estimating the deformation fields, we included a rough prior on the
 3 initial density distribution $\hat{\rho}$. This prior was then improved by incorporating the
 4 computed motion information in the image reconstruction step. The next step is
 5 to study the joint parameter identification problem, i.e. to address the challenging
 6 task of recovering $\hat{\rho}$ directly from (13) with the usual boundary conditions and the
 7 data constraint $\mathcal{A}_\Phi \hat{\rho} = g$.

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